# Midterm Examination Number Three Administered: Friday-Monday, April 9-12, 1999

## Problem 1.

Consider an isothermal flash tank:



This unit takes a pressurized liquid, three-component feed stream and exposes it to a low pressure vessel maintained under isothermal conditions. The net result is that some of the fluid is vaporized, while some fluid remains liquid. The compositions of the liquid and vapor phase are determined by the combined analysis of mass balances and Raoult's Law for vapor-liquid equilibrium.

The temperature in the flash tank is T = 298K and the pressure in the tank is P = 101kPa.

Raoult's Law states that the product of the liquid mole fraction of component i and the vapor pressure of component i is equal to the partial pressure of component i in the vapor phase:

$$x_i P_i^{vap} = y_i P$$

For Problem 1, Use the following data for the temperature given above

$$P_A^{vap} = 0.6bar @ T = 298K$$
  
 $P_B^{vap} = 1.0bar @ T = 298K$   
 $P_C^{vap} = 2.0bar @ T = 298K$ 

 $F = 100 \text{ mol/hr} \quad V = 44.738 \text{ mol/hr} \quad L = F - V \text{ mol/hr} \\ z_A = 0.4 \qquad y_A = ? \qquad x_A = ?$ 

$z_{B} = 0.3$	y <sub>B</sub> = ?	x <sub>B</sub> = ?
$z_{\rm C} = 0.3$	y <sub>C</sub> = ?	x <sub>C</sub> = ?

Then you have six unknowns, the compositions of the liquid stream and the composition of the vapor stream. (a) Write equations which will yield the unknowns. Clearly identify the origin of each equation (mass balance, constraint, Raoult's Law)

(b) Convert these equations to a linear form with unknown terms on the left hand side and constants on the right hand side, if they are not already in that form.

(c) Convert the equations to matrices and vectors.

(d) Compute the determinant and rank of the matrix, and list the random values of F and L used in the calculation.(e) Using MATLAB linear algebra functions, solve for the steady-state values of the unknown compositions.

Show MATLAB code.

(Hint: since you have 3 components, you will have three mass balances. You also have 2 streams with constraints that the sum of the mole fractions must be unity. You also have 3 Raoult's Law constraints Therefore, you have8 equations. However, you only have 6 unknowns. Not all of the 8 equations are independent. You must choose 8 independent equations. Part (d) should indicate to you whether you have selected 6 independent equations.)

### Solution:

(a)	Write equation	18							
	A mole ba	alance:		$0 = Fz_A -$	-Lx <sub>A</sub> - \	/y <sub>A</sub>			
	B mole ba	alance:		$0 = Fz_B -$	-Lx <sub>B</sub> − V	$y_{B}$ (not used, o	dependent)		
	C mole ba	alance:		$0 = Fz_C - Lx_C - Vy_C$ (not used, dependent					
	liquid mo	le fraction con	nstraint:	$1 = x_A + x_A$	$x_{B} + x_{C}$				
	vapor mo	le fraction cor	straint:	$1 = y_{A} + y_{A}$	у <sub>в</sub> +у <sub>С</sub>				
	A equilib	rium constrair	nt:	$x_A P_A^{vap} = y_A P$					
	B equilibre	rium constrair	it:	$x_B P_B^{vap} =$	$x_B P_B^{vap} = y_B P$				
	C equilibr	rium constrair	nt:	$x_{C}P_{C}^{vap} =$	∍y <sub>C</sub> P				
(b)	Put equations	in linear form							
	A mole balance:		$Lx_A + Vy_A = Fz_A$						
	B mole ba	alance:		$Lx_{B} + Vy_{B} = Fz_{B}$ (not used, dependence)			dent)		
	C mole ba	alance:		$Lx_{C} + Vy_{C} = Fz_{C}$ (not used, dependence)			dent)		
	liquid mo vapor mo	liquid mole fraction constraint: vapor mole fraction constraint:			$x_A + x_B + x_C = 1$ $y_A + y_B + y_C = 1$				
	A equilibr	A equilibrium constraint:			$x_A P_A^{vap} - y_A P = 0$				
	B equilibr	B equilibrium constraint:			$x_B P_B^{vap} - y_B P = 0$				
	C equilibr	rium constrair	nt:	$x_{C}P_{C}^{vap} - y_{C}P = 0$					
(c )	Put equations matrix of	in matrix form coefficients, A	n A (6 x 6)						
eqn/	<sup>var</sup> X <sub>A</sub>	х <sub>В</sub>	x <sub>C</sub>	У <sub>А</sub>	У <sub>В</sub>	У <sub>С</sub>			
1	L	0	0	V	0	0			
2	0	L	0	0	V	0			
5	0	U 1	L	U	0	V			
4 5	1 0	1 0	1 0	1	1	1			

$P^{vap}_A$	0	0	-P	0	0
0	$P^{vap}_B$	0	0	-P	0
0	0	$P^{vap}_C$	0	0	-P
right hand si	des, b (6x1)				
		b			
		Fz <sub>A</sub>			
		Fz <sub>B</sub>			
		Fz <sub>C</sub>			
		1			
		1			
		0			
		0			
		0			
	PA <sup>vap</sup> 0 Fright hand si	P <sub>A</sub> <sup>vap</sup> <sup>0</sup> <sup>0</sup> P <sub>B</sub> <sup>vap</sup> <sup>0</sup> 0	$\begin{array}{c c} P_{A}^{vap} & 0 & 0 \\ 0 & P_{B}^{vap} & 0 \\ 0 & 0 & P_{C}^{vap} \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

(d) Compute the determinant and rank of the matrix.

The rank of the 8 x 6 matrix written above is 6. Therefore, we need only 6 equations. I knocked out 2 of the mass balances (the second and the third) and obtained the matrix below. The rank was still 6 so I knew that I had a set of independent equations.

A =[55.2620 0 0 44.7380 0 0 1.0000 1.0000 1.0000 0 0 0 0 0 0 1.0000 1.0000 1.0000 0.6000 0 0 -1.0132 0 0 0 1.0000 0 -1.0132 0 0 0 0 0 2.0000 0 -1.0132] b =[40;1;1;0;0;0] rankA =6 detA =-83.9346 F = 100;V = 44.738;L = F - V;zA = 0.4;zB = 0.3;zC = 0.3;PvapA = 0.6;PvapB = 1.0;PvapC = 2.0;

P = 1.01325;

```
A = [L 0 0 V 0 0]
8
  0 L 0 0 V 0
   0 0 L 0 0 V
%
   1 1 1 0 0 0
   0 0 0 1 1 1
   PvapA 0 0 -P 0 0
   0 PvapB 0 0 -P0
   0 0 PvapC 0 0 -P]
%b =[F*zA; F*zB; F*zC; 1; 1; 0; 0; 0]
b = [F*zA; 1; 1; 0; 0; 0]
rankA = rank(A)
detA = det(A)
x = A \setminus b
xA = x(1);
xB = x(2);
xC = x(3);
yA = x(4);
yB = x(5);
yC = x(6);
f(1) = L^*xA + V^*yA - F^*zA;
f(2) = L*xB + V*yB - F*zB;
f(3) = L*xC + V*yC - F*zC;
f(4) = yA + yB + yC - 1.0;
f(5) = xA + xB + xC - 1.0;
f(6) = PvapA*xA - P*yA;
f(7) = PvapB*xB - P*yB;
f(8) = PvapC*xC - P*yC;
x = [0.4893
 0.3018
 0.2090
 0.2897
 0.2978
 0.4125]
                               X<sub>C</sub>=0.2090
X_{A} = 0.4893 X_{B} = 0.3018
y<sub>A</sub>=0.2897 y<sub>B</sub>=0.2978
                               y_{c} = 0.4125
```

Problem 2.

Consider the same flash tank describe in Problem (1). Now consider that the L and V stream flowrates are also unknowns. This makes the problem a set of 8 non-linear equations. Use systems or the MATLAB program of your choice to solve for liquid and vapor stream compositions and flow-rates. Use an initial guess of

**x**<sub>A</sub>=0.33 **x**<sub>B</sub>=0.33 **x**<sub>C</sub>=0.33

y<sub>A</sub>=0.33 y<sub>B</sub>=0.33 y<sub>C</sub>=0.33

$$L = 50$$
  $V = 50$ 

Show your input file, sysequinput.m. Show your answer. Clearly indicate which variables are which.

# Solution:

sysequ	n([0.33,0	).33,0.33,	0.33,0.33	3,0.33,50,50]	)
VARI	ABLE	INPUT	OUTP	UT	
1	3.30000	000e-001	4.89274	70e-001	
2	3.30000	000e-001	3.01765	42e-001	
3	3.30000	)00e-001	2.08959	88e-001	
4	3.30000	)00e-001	2.89725	95e-001	
5	3.30000	)00e-001	2.97819	31e-001	
6	3.30000	)00e-001	4.12454	73e-001	
7	5.00000	000e+001	4.47382	291e+001	
8	5.00000	000e+001	5.52617	709e+001	

- $x_{A} = 0.4893$   $x_{B} = 0.3018$   $x_{C} = 0.2090$
- y<sub>A</sub>=0.2897 y<sub>B</sub>=0.2978 y<sub>C</sub>=0.4125
- V =44.738 mol/hr L =55.262 mol/hr

## Problem 3.

In an isothermal batch reactor, the following reaction occurs:  $A + 2B \rightarrow C$ 

You know the initial concentrations of A, B, and C:  $A_0$ ,  $B_0$ , and  $C_0$ . You record the concentration of C, C(t), as a function of time, t.

You repeat the experiment for several different temperatures, T. (Thus you have the concentration as a function of time and temperature.)

From kinetics, you know the rate of production of C is given by:

$$rate(t) = \frac{dC(t)}{dt} = A \cdot B^2 \cdot k_o \exp^{\frac{-Ea}{RT}} = (A_o - C) \cdot (B_o - 2C)^2 \cdot k_o \exp^{\frac{-Ea}{RT}}$$

You want to perform a regression to obtain the reaction rate constant,  $k_0$  and the activation energy,  $E_a$ 

but you couldn't measure the rate,  $\frac{dC(t)}{dt}$ , only the concentration C(t). (This is how the process usually works). To handle this, you can rearrange and analytically integrate this differential equation to yield:

$$k_{o} \exp^{\frac{-Ea}{RT}} t = \left(\frac{-2}{(B_{o} - 2A_{o})^{2}}\right)^{2} \left\{ 2(B_{o} - 2A_{o})\left(\frac{1}{B_{o} - 2C} - \frac{1}{B_{o} - 2C_{o}}\right) - 2\ln\left(\frac{B_{o} - 2C}{B_{o} - 2C_{o}}\right) + \frac{1}{2}\ln\left(\frac{A_{o} - C}{A_{o} - C_{o}}\right) \right\}$$

(a) Put this equation in a form like  $y = b_0 + b_1 x$  so that you could perform least squares linear regression on it to determine the reaction rate constant,  $k_0$  and the activation energy,  $E_a$ , from data which gives Clearly identify all four variables in this equation,  $y = b_0 + b_1 x$ . Clearly identify how to obtain  $k_0$  and  $E_a$  from the fit constants.

(b) Download the data file, xm03file.zip from the Homeworks section of the course website. This file has been zipped with WinZip. You must unzip the file using the WinZip utility, available on the computers in Dougherty 314. Once the file has been unzipped, you can read the data as an Excel spreadsheet, which gives concentration as a function of time and temperature. From this data, calculate

- (a)  $\mathbf{k}_{o}$  and  $\mathbf{E}_{a}$
- (b) the standard deviations of  $k_0$  and  $E_a$

(c) the measure of fit of the model. Clearly indicate all answers. Do not simply provide an ambiguous program output.

### Solution:

» regress(1,1,80,1,'file.x3p3s99.dat') COMPLETED A LINEAR REGRESSION ON THE DATA IN file.x3p3s99.dat THE NUMBER OF PARAMETERS IS 2 The zeroth order parameter was used. THE NUMBER OF DATA POINTS IS 80 PARAMETER VALUE STANDARD DEVIATION 1 1.4057494e+001 1.2257327e+000 2 3.5765021e+004 2.9793620e+003 MOF = 6.4881022e-001F = 1.4410214e+002degrees of freedom = 7.8000000e+001

$$k_o = \exp(b_o) = \exp(14.057494) = 1.27 \cdot 10^6$$
  
 $E_a = b_1 = 35765.021$ 

 $\sigma_{k_{\Omega}} = \sigma_{exp(b_{\Omega})} \approx exp(\sigma_{b_{\Omega}}) = 3.41$ 

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$$\sigma_{E_a} = \sigma_{b_1} = 2979.362$$

Measure of Fit = MOF = 0.64881022